Amendments to the Specification

Please replace the paragraph starting on line 5, page 12 with the following:

Figures 7B to 8D show examples of a third inventive mechanisms for reducing TMR. This includes moving the actuator arm by the lever action through the principal axis when the slider is parallel to the disk surface. The slider is mounted on a flexure at a second bias angle ~~710~~ 712 to the principal axis. The means for radially moving the slider includes the flexure responding as the disk surface bends through the second bias angle, causing the slider to move radially toward the track.

Please replace the paragraph starting on line 11, page 12 with the following:

Figure 7B shows a top view of the suspension attached to base plate 70, with two points 722 and 724 welding flexure 90 to load beam 80, providing second bias angle ~~710~~ 712. Flexure 90 attaches to both slider 100 and to load beam 80. The number of welding points close to the slider is preferably at least two. If the line between welding points is not perpendicular to the principal axis 110, then the trajectory of bending motion of the flexure induced by disk axial vibration will be on a tilted bending line. It is sometimes preferred that the line, between the welding points 722 and 724, is not perpendicular to the principal axis 110.

Please replace the paragraph starting on line 17, page 13 with the following:

Figures 14A and 14B show the geometric analysis used for the second bias angle ~~710~~ 712 formula for the mechanisms of Figures 7B to 8D when the disk surface bends down as in Figure 11A and bent up as in Figure 11C. In these Figures:

Please replace the paragraph starting on line 22, page 13 with the following:

φ refers to the roll bias angle, also the second bias angle which is portrayed in Figures 7B to 8D by reference number ~~710~~ 712.

Please replace the paragraph starting on line 7, page 14 with the following:

The bias angle 710 and the second bias angle 712 of the earlier Figures is the roll bias angle φ of Figures 14A-16C. In Figure 14A, the roll bias angle φ = arc cos((a - b cos θ) / c) for the disk bending down. In Figure 14B, the roll bias angle φ = arc cos((b cos θ - d) / c) for the disk bending up. This leads to $\varphi \approx$ 1.2 degrees of arc at the Outside position of Disk OD, with r = 45 mm. In Figures 14A and 14B, the radial motion of slider 100 is about h = b * sin θ = (ts+td/2) sin θ.